

Development of a New Generation Low Cost Treatment of Ammonia for Livestock Effluents Using Anammox and Nitritation

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Introduction

The environmental problems due to confined animal feeding operation (CAFOs) are under concern around the world in the last years. Among CAFOs, the swine production wastewater are very significant due to its high nutrient concentration, mainly phosphorous and nitrogen (Kunz et al., 2005). Specifically for nitrogen, its high concentration in water, contribute to the toxicity of life organisms, depletion of dissolved oxygen, risks to public health and, associated with phosphorous, to the eutrophization phenomena (Bitton, 2005).

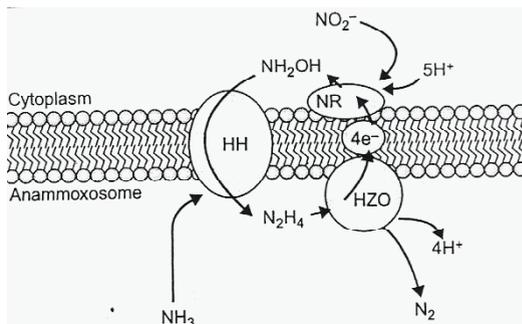
Based in these facts, when it is no sufficient soil to use it as a fertilizer, the necessity of treatment is necessary. The main problem is that nitrogen is an specie that is very difficult to remove from swine manure by classical treatment processes. Nitrification/denitrification processes, have some limitations to be used to swine manure, as an inhibition by some species that are formed during the degradation process needing a high control of nitrification/denitrificaton.

New paths to remove nitrogen from effluents have been developed in last years, as the process of anaerobic ammonia oxidation (ANAMMOX). In this process ammonio (NH_4^+) are directly oxidized to gaseous nitrogen (N_2) and nitrite (NO_2^-), is the final electron acceptor. The process is autotrophic and use CO_2 as a carbon source. Nitrate (NO_3^-) is the by-product and the process global stechiometry is described bellow (Strous et al. (1998)):



In this metabolic rote, the nitrite is reduced to hydroxylamine that react with ammonium producing gaseous nitrogen. Figure 1 presents a suggestion of anammox reactions in cytoplasm. Part of this reactions occur inside the bacteria cellular compartment named Anammoxosome (Jetten et al. 2000).

Figure 1: Ammonium anaerobic oxidation mechanism. NR= nitrite reducing enzyme; HH= hydrazine hydrolase; HZO= hydrazine oxidacing enzyme (AHN, 2006)



It were identified sludges with anammox activities around the world, (Den Camp et al, 2006, Vanotti et al., 2006) showing a development characteristics of microorganisms in a different habitats.

The big challenge to anammox good activity is to supply ammonium and nitrite in the stoichiometric microorganism necessity. Anammox bacteria use ammonia and nitrite. Therefore, nitrification as the preceding treatment step of Anammox should be partial in that only about 50% of the ammonia needs to be oxidized, and the oxidized N should be mostly nitrite (by preventing the conversion of nitrite to nitrate). Although various approaches have been proposed for achieving partial nitritation, there is still a need for more effective and economical processes. The SHARON process is an effective partial nitritation process. It is based on the higher growth rate of ammonia oxidizing bacteria (*Nitrosomonas* sp.) relative to nitrite oxidizing bacteria (*Nitrobacter* sp.) obtained at high process temperatures ($> 30\text{ }^{\circ}\text{C}$) and the subsequent disappearance or washout of *Nitrosomonas* sp. with short retention times. But heating of the water is very expensive and may be impractical in many situations. Another approach for partial nitritation has been the use of low DO concentrations and the higher affinity of *Nitrosomonas* sp. for oxygen leading to accumulation of nitrite. However, maintaining stable nitrite production using the low DO approach has been difficult to achieve in wastewater treatment plants. Our approach for partial nitritation was the inhibition of *Nitrobacter* to free ammonia using pH control.

One mechanism by which pH affects the rate of nitrification has been proposed by Anthonisen et al. (1976). They proposed that nitrifying bacteria are inhibited by the un-ionized rather than the total ion concentration of ammonia and nitrite. Their studies showed that NH_4^+ oxidation by *Nitrosomonas* sp. is usually inhibited at concentrations of un-ionized nitrous acid (HNO_2) of 0.2 to 2.8 mg L^{-1} and concentration of un-ionized ammonia (NH_3) of 10 to 150 mg L^{-1} , while NO_2^- oxidation by *Nitrobacter* sp. is inhibited with NH_3 concentrations in the range of 0.1 to 1.0 mg L^{-1} . In studies of nitrification of swine wastewater, Vanotti and Hunt (2000) obtained effective inhibition of *Nitrobacter* sp. when NH_3 exceeded 2.0 mg L^{-1} . These inhibitory conditions should be relatively easy to obtain in practical treatment of livestock effluents or other high-ammonia effluents because for example a liquid with a total $\text{NH}_4\text{-N}$ concentration of 230 mg L^{-1} and a pH of 8.3 contains $38.7\text{ mg NH}_3\text{ L}^{-1}$.

Material and Methods

Anammox

Inoculum. The sludge for this study was collected from the bottom of an inactive anaerobic lagoon in experimental swine manure treatment lagoons at Embrapa's Swine and Poultry, Concordia, SC, Brazil.

Acclimation. The sludge was screened, washed with water, and kept in a KNO_3 (100 mg L^{-1}) solution until the denitrification process stopped, that is a good indication that the organic carbon was consumed. After this initial acclimation, the sludge was inoculated in an anammox reactor.

Reactor set-up

The sludge was inoculated at 4 g/L TSS in a 2 L reactor. The process was kept at $35\text{ }^{\circ}\text{C}$ and pH 7. The feeding medium was prepared according to Shierholt Neto et al. (2006). To remove the interference of oxygen in the process, N_2 was bubbled until dissolved oxygen concentration was 0.5 mg/L . The Hydraulic Retention Time (HRT) was adjusted between 18.5 h and 24 h.

Partial nitrification

Reactor set-up

The reactor consisted of a 5-L aeration tank containing 600 mL of porous PVA beads (Kurarey Co., Japan) used for attachment of the nitrification bacteria. The reactor had a divider to allow up and down circulation of the beads. A 1-mm screen was placed before the outlet port to separate the beads and free cells, and retain the beads inside the reactor. Air was supplied from the bottom of one half of the tank at a flow rate of 0.8 L min^{-1} to ensure full fluidization of immobilized pellets. The diffuser consisted of an aquarium porous stone that provided fine bubble aeration. A variable flow peristaltic pump was used in the continuous flow experiments to feed the wastewater to the nitrification tank. The $\text{NH}_4\text{-N}$ loading rate was adjusted by varying the flow rates from 2500 to 5000 mL d^{-1} . A pH controller and an injection pump was used to control the process pH using 2 mol L^{-1} NaOH at set points of 7.5, 8.5, 8.7 and 8.9. The reactor was inoculated with 70 mL of nitrifying sludge acclimated to livestock wastewater and operated first under batch mode during approximately 20 days using a fill-and-draw technique to facilitate attachment and growth of a nitrifying biofilm on the surface of the beads. The reactor was then operated under continuous flow with a synthetic medium (Vanotti and Hunt, 2000) containing 700 ppm of $\text{NH}_4\text{-N}$. The process pH was increased gradually in the range of 7.5-8.9 to study the pH effect on partial nitritation at low temperatures ($22 \text{ }^\circ\text{C}$).

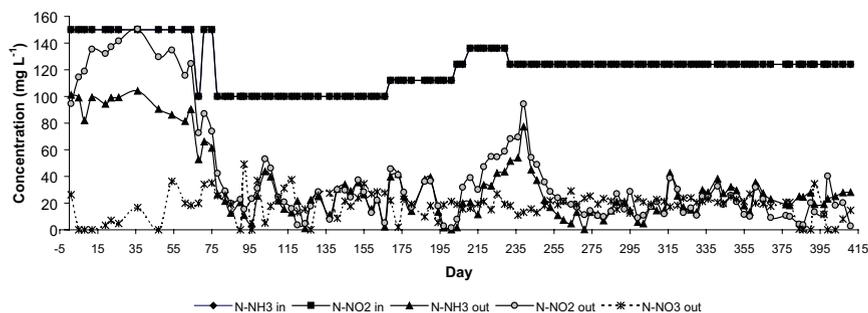
Chemical analyses

All chemical analyses were done according to APHA (1995). Liquid samples from the reactor (in and out) were taken twice a week and analyzed for N-NH_3 , N-NO_2 , N-NO_3 using Flow Injection Analysis (FIALAB INSTRUMENTS). Alkalinity was determined by titration with H_2SO_4 0.02 mol/L until pH 4.5.

Results and Discussion

The anammox reactor (Figure 2) took around 75 days to start to develop a anammox activity with a fast decrease of nitrite and ammonia concentration in the reactor effluent. The system is working in a very stable conditions for around a year, excepting around the day 235 when an anammox inhibition activity was developed, probably due to the effect of increase in nitrite concentration (Dapena-Mora et al. 2006).

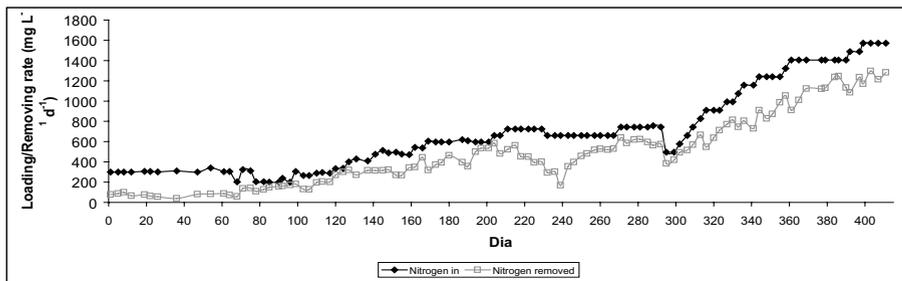
Figure 2: Nitrogen conversion in anammox reactor during the operation time



A high nitrogen removal capacity of anammox reactor was reached (Figura 3) mainly after 300 days of operation when the reactor was feeding with a nitrogen loading rate around $1600 \text{ mg L}^{-1} \text{ d}^{-1}$. The nitrogen removal efficiency of anammox system is very high when compared to classical N removal system as nitrification and denitrification reactors. This

make possible to conclude that we can have smaller anammox reactors working with high efficiency reducing the cost with reactor constructions.

Figure 3: Nitrogen Loading/removing rate in the anammox reactor



The partial nitrification reactor was stabilized in a few weeks during a batch experiment establishing first of all the complete nitrification process. After this the reactor was operated as a continuous form and the pH was increased. A desired partial nitrification, 50 % ammonia oxidation was reached between pH 8.5 –8.9. This is a important result and make able a connection between anammox and a partial nitrification reactor.

Acknowledgements

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